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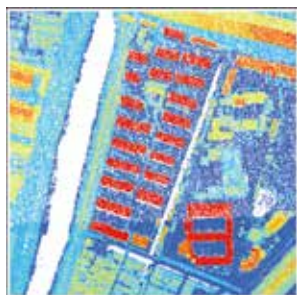
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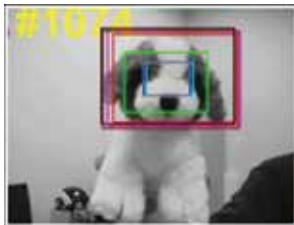
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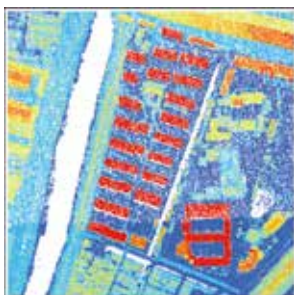
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基于全正基的非均匀三次加权 B 样条

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摘要: 目的 对 B 样条的改进方法大多从增加局部参数和在三角函数空间定义基两个角度出发, 但仍存在缺陷, 原因是通过模型的控制顶点对曲线进行编辑和处理, 存在控制顶点给定时曲线较为固定的不足。为此, 本文构造了一类基于全正基的非均匀三次加权 $\lambda\alpha\beta$ -B 样条基。方法 结合加权思想, 首先证明三次有理基在相应空间上的全正性; 其次对三次三角基和三次有理基同时进行扩展, 得到新的 $\lambda\alpha\beta$ -B 样条基, 新扩展基具有和经典 B 样条基相似的性质; 最后对新扩展基进行线性组合, 用得到的多项式构造非均匀三次加权 $\lambda\alpha\beta$ -B 样条基, 并研究了曲线的定义及性质。结果 实验结果表明, 新曲线保留传统 B 样条曲线基本性质的同时, 还具有局部调整性, 可以改善只通过调整控制顶点改变曲线形状的不足。结论 构造的新 $\lambda\alpha\beta$ -B 样条曲线可以有效克服传统方法在改进时的不足, 适合曲线设计。

关键词: $\lambda\alpha\beta$ -Bernstein 基; 加权 $\lambda\alpha\beta$ -B 样条; 非均匀; 全正性; 局部调整性质

Non uniform weighted cubic B-spline based on all positive basis

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Abstract: Objective The construction of B-spline basis functions has always been the focus of computer-aided design. The purpose of its research is mainly to solve the problem that the curve generated by the traditional method is fixed relative to the control vertices. The transformation form mainly incorporates the shape into the constructed basis function parameters to increase the flexibility of the curve, that is, to introduce free parameters to the expression of the classic Bernstein basis function or the extended Bernstein basis function, and adjusts the value of the parameter to adjust the shape of the curve. In recent years, researchers have proposed a large number of B-spline improvements, and they are mainly focused on two function spaces, namely, polynomial function space and trigonometric function space. The spline basis functions constructed in these two function spaces have their own advantages in addition to local adjustments to the corresponding curves. The spline curve constructed in the polynomial function space can be degenerated into a classic B-spline curve and has the advantages of simple calculation. Conversely, the basis function constructed in the trigonometric function space has the advantage of the derivation and cyclability of the trigonometric function. Both have high-order continuity, enabling the accurate representation of circle, ellipse, parabola, sine, cosine, cylindrical spiral, etc. The main purpose of this study is to combine the

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advantages of constructing spline basis functions in these two function spaces and use the weighting method to integrate the basis functions constructed in the two function spaces. The newly introduced weighting factors can be used as global parameters to make new extensions, and the flexibility of the curve is further enhanced. However, from the above two perspectives, some defects still exist. The reason is that the curve is edited and processed through the control vertices of the model, similar to the traditional method. When the control vertices are given, the curve is relatively fixed. **Method** First, construct a set of cubic rational basis functions in the polynomial function space and prove that they are fully positive. Then, use the weighting idea to weigh the newly constructed cubic rational basis functions and the cubic triangular basis functions constructed and new Bernstein basis and prove that it retains all the good properties of the classic Bernstein basis functions. Subsequently, the new extended basis is linearly combined to obtain the non-uniform cubic weighted B-spline basis, and its properties are studied. Finally, the definition and properties of the corresponding cubic spline curve are given, and the application of the new curve is given based on it. **Result** Experiments show that the curve constructed by the weighting method in this study retains the respective advantages of the polynomial function space and the trigonometric function space and also has local adjustment. At the same time, the introduced weighting factor also strengthens its global adjustment and further enhances the flexibility of the generated curve. It can improve the shortcomings of changing the curve shape only by adjusting the control vertices. **Conclusion** In this study, the new $\lambda\alpha\beta$ -B-spline curve constructed by the weighting method has a structure similar to the classic B-spline curve while retaining the same properties as the classic B-spline curve, such as convex hull, symmetry, geometric invariance, and change. In addition, the curve constructed by the weighting method in this paper has some unique advantages: first, it has two local shape parameters that can be adjusted locally; second, the weighting factor introduced can be used as a global parameter, and the generated $\lambda\alpha\beta$ -B-spline curve can perform global adjustment; third, the $\lambda\alpha\beta$ -B-spline curve constructed by the weighting method retains the respective advantages of the polynomial function space and the trigonometric function space. The results show that the shape parameter selection scheme of the constructed curve is correct and effective, which reflects the superiority of the method in this study over other similar methods in the literature. In addition, the construction method with parameter expansion base given in this study and the selection method of shape parameters are general, which can be extended to construct B-spline and triangle surfaces with shape parameters.

Key words: $\lambda\alpha\beta$ -Bernstein basis; weighted $\lambda\alpha\beta$ -B-spline; non-uniform; total positive; local adjustment property

0 引言

曲线曲面是计算机辅助几何设计 (computer aided geometric design, CAGD) 研究的重要内容之一,在飞机、汽车和船体等外形设计上具有广泛应用。常用的是 Bézier 方法 (师利红和张贵仓, 2011; 汪凯等, 2018; 吴晓勤等, 2008) 和 B 样条方法 (韩旭里和刘圣军, 2003; 王文涛和汪国昭, 2004; 张贵仓和耿紫星, 2007), Bézier 方法具有仿射不变性、几何直观性、变差缩减性等很多优良性质,但存在缺乏灵活性、控制性差和不易修改等不足。B 样条方法保留了 Bézier 方法的优点,克服了 Bézier 方法的缺陷,最大优点是若改变某一控制点的顶点值,只影响下一个顶点,不会影响整条拟合函数。由于实际问题复杂,传统的 B 样条方法已无法满足实际需求,于是在传统 B 样条方法上提出了非均匀有理 B 样条

(non-uniform rational B-splines, NURBS) 方法,但是其权因子并未解决。对此有两方面的改进:1) 利用参数方法表示曲线曲面,可以不利用坐标系而仅使用计算机实现,方便快捷;2) 将基函数定义在非多项式空间、三角函数空间 (耿紫星和张贵仓, 2008; 严兰兰等, 2016; 陈素根等, 2015; 尹池江和檀结庆, 2011) 或双曲函数空间 (张锦秀和檀结庆, 2011; 郭弘毅和左华, 2007; 方玲和王旭辉, 2016) 上,使相应曲线在具备 B 样条方法类似性质的同时,可以利用三角函数求导的特殊性 (即 $\sin^{(4)}t = \sin t$, $\cos^{(4)}t = \cos t$) 表示圆锥曲线等超越曲线。

由于非均匀节点的非等距分布,非均匀 B 样条基在改进方法上存在一定困难,大多数都以均匀 B 样条为主,但未能得到广泛应用,原因主要有:1) 这些改进方法使用的大多是全局参数,并不具备局部控制性;2) 只证明了一些如凸包性、仿射不变性、端点插值等基本性质,像变差缩减、保凸性等重要性

质未给出证明;3)改进方法大多以节点等距为主,对非等距节点并未讨论。

陈福来等人(2012)给出了多项式空间中一组含参数的三次有理基,但未证明该基是全正基。本文首先证明了该三次有理基是相应空间上的最优规范全正基,所以由该基构成的非均匀三次有理 B 样条曲线具有变差缩减性和保凸性质,能更好地支配多边形的形态;其次由于三角函数求导的可循环性,其优点是在一定条件下可以精确表示圆弧、椭圆弧和抛物线弧等二次曲线弧。若想同时保留有理基和三角基的优点,本文对其进行扩展,结合加权思想,得到了新的 $\lambda\alpha\beta$ -Bernstein 基,最后用扩展基的线性组合表示扩展 B 样条基即非均匀 $\lambda\alpha\beta$ -B 样条基,并给出了曲线的定义,证明了其重要性质。结果显示,本文构造的非均匀加权 $\lambda\alpha\beta$ -B 样条曲线解决了传统 B 样条曲线在局部控制上的问题,适合曲线设计。

1 相关知识

1.1 基础知识

若对于任意的节点序列 $a \leq t_0 < t_1 < \dots < t_n \leq b$, 基函数 $(u_0, u_1, \dots, u_n)$ 的配置矩阵 $u_i(t_i)$, $0 \leq i \leq n$ 是一个全正矩阵,即矩阵 $(u_i(t_i))$ 的任意一个子矩阵的行列式是非负的,则称基函数 $(u_0, u_1, \dots, u_n)$ 为闭区间 $[a, b]$ 上的全正基。对于一个含有全正基的函数空间,其余全正基可以由一组全正基乘以全正转换矩阵得到(朱远鹏,2014)。

1.2 非均匀三次三角 B 样条基

Han 和 Zhu(2014)给出了当 $\beta \in [0, 1]$, $t \in [0, 1]$, 时,构造的三次三角基,具体为

$$\begin{cases} B_0(t) = \left(1 - \sin \frac{\pi t}{2}\right)^2 \left(1 - \beta \sin \frac{\pi t}{2}\right) \\ B_1(t) = \sin \frac{\pi t}{2} \left(1 - \sin \frac{\pi t}{2}\right) \left(2 + \beta - \beta \sin \frac{\pi t}{2}\right) \\ B_2(t) = \cos \frac{\pi t}{2} \left(1 - \cos \frac{\pi t}{2}\right) \left(2 + \beta - \beta \cos \frac{\pi t}{2}\right) \\ B_3(t) = \left(1 - \cos \frac{\pi t}{2}\right)^2 \left(1 - \beta \cos \frac{\pi t}{2}\right) \end{cases} \quad (1)$$

汪凯等人(2019)在式(1)的基础上,定义了一类带一个形状参数的非均匀三次三角 B(cubic trigo-

nometric B, CT-B) 样条基,具体为

$$G_i(u) = \begin{cases} G_{i,0}(t_i) = n_i B_3(t_i; \beta_i) & u \in [u_i, u_{i+1}) \\ G_{i,1}(t_{i+1}) = \sum_{j=0}^3 m_{i+1,j} B_j(t_{i+1}; \beta_{i+1}) & u \in [u_{i+1}, u_{i+2}) \\ G_{i,2}(t_{i+2}) = \sum_{j=0}^3 y_{i+2,j} B_j(t_{i+2}; \beta_{i+2}) & u \in [u_{i+2}, u_{i+3}) \\ G_{i,3}(t_{i+3}) = x_{i+3} B_0(t_{i+3}; \beta_{i+3}) & u \in [u_{i+3}, u_{i+4}) \\ 0 & u \notin [u_i, u_{i+4}) \end{cases}$$

式中, $B_j(t_i; \beta_i)$ ($j = 0, 1, 2, 3$) 为式(1)中给出的基函数,其他系数为

$$\begin{aligned} \mu_i &= 2(2\beta_i + 1)(\beta_i + 2)(h_i + h_{i+1}) \\ \nu_i &= 2(\beta_i + 2)(h_i + h_{i+1}) \\ v_i &= \frac{\mu_i h_i + \nu_i h_{i+1}}{(\beta_i + 2)h_{i+1}^2} \\ \omega_i &= \frac{\mu_{i-1} h_i + \nu_{i-1} h_{i-1}}{(\beta_{i-1} + 2)h_{i-1}^2} \\ x_i &= \frac{(\beta_{i-1} + 2)\mu_{i-2} h_i^2}{\mu_{i-1}\nu_{i-2}h_{i-2} + \mu_{i-2}\mu_{i-1}h_{i-1} + \mu_{i-2}\nu_{i-1}h_i} \\ n_i &= \frac{(\beta_i + 2)\mu_{i+1} h_i^2}{\mu_{i+1}\nu_i h_i + \mu_i \mu_{i+1} h_{i+1} + \mu_i \nu_{i+1} h_{i+2}} \\ y_{i,0} &= \frac{(\beta_{i-1} + 2)\nu_i h_{i-1}}{\nu_{i-1}} x_{i+1} + \frac{(\beta_{i-1} + 2)\omega_{i-1} h_i}{\nu_{i-1}} n_{i-2} \\ y_{i,1} &= \nu_i x_{i+1} \\ m_{i,0} &= n_{i-1} \\ y_{i,2} &= \frac{\nu_i}{(\beta_i + 2)h_{i+1}} x_{i+1} \\ m_{i,1} &= \frac{\nu_{i-1}}{(\beta_{i-1} + 2)h_{i-1}} n_{i-1} \\ y_{i,3} &= x_{i-1} \\ m_{i,2} &= \omega_i n_{i-1} \\ m_{i,3} &= \frac{(\beta_i + 2)\nu_{i+1} h_i}{\nu_i} x_{i+2} + \frac{(\beta_i + 2)\omega_{i+1} h_{i+1}}{\nu_i} n_{i-1} \end{aligned}$$

2 非均匀三次有理 B 样条基

2.1 非均匀三次有理 B 样条基的构造

陈福来等人(2012)构造了一类带两个参数的三次有理多项式基函数,具体为

$$\begin{cases} I_0(t) = (1-t)^2(1-\alpha t) \\ I_1(t) = (2+\alpha)t(1-t)^2 \\ I_2(t) = (2+\beta)t^2(1-t) \\ I_3(t) = (1-\beta+\beta t)t^2 \end{cases}$$

式中, $\alpha, \beta \in (0, 1]$, $t \in [0, 1]$ 。朱远鹏(2014)分析了基函数的非负性、规范性和拟对称性等性质,但未讨论全正性。

本文定义基函数 $\{I_i(t)\}$ 为带一个形状参数的三次有理基 $\{A_i(t)\}$, 并对其全正性进行分析。

定义1 对于 $\forall \alpha \in [0, 1]$, $t \in [0, 1]$, 称以下表达式为三次有理基

$$\begin{cases} A_0(t) = (1-t)^2(1-\alpha t) \\ A_1(t) = (2+\alpha)t(1-t)^2 \\ A_2(t) = (2+\alpha)t^2(1-t) \\ A_3(t) = (1-\alpha+\alpha t)t^2 \end{cases} \quad (2)$$

从 $\{A_i(t)\}$ 的表达式不难发现, $\{A_i(t)\}$ 可用经典三次 Bernstein 基 $V_{i,n}(t) = C_3^i t^i (1-t)^{3-i}$, $i = 0, 1, 2, 3$ 表示, 即 $(A_0(t), A_1(t), A_2(t), A_3(t)) = (V_0(t), V_1(t), V_2(t), V_3(t))L$, 其中,

$$L = \begin{pmatrix} 1 & 0 & 0 & 0 \\ \frac{1-\alpha}{3} & \frac{2+\alpha}{3} & 0 & 0 \\ 0 & 0 & \frac{2+\alpha}{3} & \frac{1-\alpha}{3} \\ 0 & 0 & 0 & 1 \end{pmatrix} \quad (3)$$

定理1 当 $\alpha \in [0, 1]$ 时, 矩阵 L 为非奇异随机全正矩阵。

证明: 对任意 $\alpha \in [0, 1]$, 显然矩阵 L 的各行和为1, 即 L 为随机矩阵。此外, 直接计算有

$$\left\{ \begin{aligned} \begin{vmatrix} 1 & 0 \\ \frac{1-\alpha}{3} & \frac{2+\alpha}{3} \end{vmatrix} &= \frac{2+\alpha}{3} > 0 \\ \begin{vmatrix} \frac{2+\alpha}{3} & 0 \\ 0 & \frac{2+\alpha}{3} \end{vmatrix} &= \left(\frac{2+\alpha}{3}\right)^2 > 0 \\ \begin{vmatrix} \frac{2+\alpha}{3} & \frac{1-\alpha}{3} \\ 0 & \frac{2+\alpha}{3} \end{vmatrix} &= \left(\frac{2+\alpha}{3}\right)^2 > 0 \end{aligned} \right.$$

据此容易看出 L 的所有子行列式均非负, 故矩阵 L 为非奇异随机矩阵。

定理2 当 $\alpha \in [0, 1]$ 时, 基函数 $\{A_i(t)\}$ 为全正基。

证明: 由于经典的三次 Bernstein 基 $V_{i,n}(t)$ 为一组最优规范全正基, 由定理1 又可知矩阵 L 为非奇异随机全正矩阵, 因此基函数 $\{A_i(t)\}$ 为全正基。

鉴于式(2)定义的三次有理基不具有形状可调性, 且在设计复杂曲线时需解决光滑拼接问题。为此, 在式(2)基础上构建一类非均匀三次有理 B(cubic rational B, CR-B) 样条基, 进行曲线设计。

对于给定的节点序列 $u_0 < u_1 < \dots < u_{n+4}$, 记为节点矢量 $U = (u_0, u_1, \dots, u_{n+4})$ 。令 $h_j = u_{j+1} - u_j$, $t_j(u) = (u - u_j)/h_j$, $j = 0, 1, \dots, n+3$ 对于任意的形状参数 $\alpha_i \in [0, 1]$, $i = 0, 1, \dots, n$ 待构造的 CR-B 样条基为

$$S_i(u) = \begin{cases} S_{i,0}(t_i) = q_i A_3(t_i; \alpha_i) & u \in [u_i, u_{i+1}) \\ S_{i,1}(t_{i+1}) = \sum_{j=0}^3 p_{i+1,j} A_j(t_{i+1}; \alpha_{i+1}) & u \in [u_{i+1}, u_{i+2}) \\ S_{i,2}(t_{i+2}) = \sum_{j=0}^3 f_{i+2,j} A_j(t_{i+2}; \alpha_{i+2}) & u \in [u_{i+2}, u_{i+3}) \\ S_{i,3}(t_{i+3}) = e_{i+3} A_0(t_{i+3}; \alpha_{i+3}) & u \in [u_{i+3}, u_{i+4}) \\ 0 & u \notin [u_i, u_{i+4}) \end{cases} \quad (4)$$

式中, $A_j(t_i; \alpha_i)$ ($j = 0, 1, 2, 3$) 为式(2)中给出的基。

为了确定系数 $e_i, f_{i,j}, p_{i,j}, q_i$ 的值, 对 CR-B 样条基进行限制: 1) $S_i(u)$ 在所有节点上均 C^2 连续; 2) $S_i(u)$ 在区间 $[u_3, u_{p+1}]$ 上具有单位性。由此经过一些运算后, 可以直接求出系数为

$$\begin{aligned} \sigma_i &= 2(2\alpha_{i+1} + 1)(\alpha_{i+1} + 2)(h_i + h_{i+1}) \\ \tau_i &= 2(\alpha_{i+1} + 2)(h_i + h_{i+1}) \\ \delta_i &= \frac{\sigma_i h_i + 3\tau_i h_{i+1}}{3(\alpha_{i+1} + 2)h_{i+1}^2} \\ \gamma_i &= \frac{\sigma_{i-1} h_i + 3\tau_{i-1} h_{i-1}}{3(\alpha_i + 2)h_{i-1}^2} \\ e_i &= \frac{3(\alpha_i + 2)\sigma_{i-2} h_i^2}{3\sigma_{i-1}\tau_{i-2} h_{i-2} + \sigma_{i-2}\sigma_{i-1} h_{i-1} + 3\sigma_{i-2}\tau_{i-1} h_i} \\ q_i &= \frac{3(\alpha_{i+1} + 2)\sigma_{i+1} h_i^2}{3\sigma_{i+1}\tau_i h_i + \sigma_i\sigma_{i+1} h_{i+1} + 3\sigma_i\tau_{i+1} h_{i+2}} \\ f_{i,0} &= \frac{(\alpha_i + 2)\delta_i h_{i-1}}{\tau_{i-1}} e_{i+1} + \frac{(\alpha_i + 2)\gamma_{i-1} h_i}{\tau_{i-1}} q_{i-2} \\ f_{i,1} &= \delta_i e_{i+1} \\ p_{i,0} &= q_{i-1} \\ f_{i,2} &= \frac{\tau_i}{(\alpha_{i+1} + 2)h_{i+1}} e_{i+1} \\ p_{i,1} &= \frac{\tau_{i-1}}{(\alpha_i + 2)h_{i-1}} q_{i-1} \\ f_{i,3} &= e_{i+1}, p_{i,2} = \gamma_i q_{i-1} \end{aligned}$$

$$p_{i,3} = \frac{(\alpha_{i+1} + 2)\delta_{i+1}h_i}{\tau_i}e_{i+2} + \frac{(\alpha_{i+1} + 2)\gamma_i h_{i+1}}{\tau_i}q_{i-1}$$

定义2 给定节点矢量 U , 对于任意 $\alpha_i \in [0, 1]$ 和上面给出的系数 $e_i, f_{i,j}, p_{i,j}, q_i$, 称式(4)为带1个参数的 CR-B 样条基。节点等距时, 称 CR-B 样条基 $S_i(u)$ 为均匀 B 样条基, 相应的节点矢量 U 称为等距节点矢量; 节点非等距时, 称 CR-B 样条基 $S_i(u)$ 为非均匀 B 样条基, 相应的节点矢量 U 称为非等距节点矢量。

引理1 对任意 $i \in \mathbf{Z}$, 下列等式成立

$$\begin{aligned} 1) & e_i + f_{i,0} + p_{i,0} = 1 \\ 2) & f_{i,1} + p_{i,1} = 1 \\ 3) & f_{i,2} + p_{i,2} = 1 \\ 4) & f_{i,3} + p_{i,3} + q_i = 1 \\ 5) & q_i = p_{i+1,0} \\ 6) & f_{i+2,0} = p_{i+1,3} \\ 7) & f_{i+2,3} = e_{i+3} \\ 8) & \left(\frac{\pi}{2h_i}\right)q_i = \left(\frac{\pi}{2h_{i+1}}\right)(p_{i+1,1} - p_{i+1,0}) \\ 9) & \left(\frac{\pi}{2h_{i+1}}\right)(p_{i+1,3} - p_{i+1,2}) = \left(\frac{\pi}{2h_{i+2}}\right)(f_{i+2,1} - f_{i+2,0}) \\ 10) & \left(\frac{\pi}{2h_{i+2}}\right)(f_{i+2,3} - f_{i+2,2}) = -\left(\frac{\pi}{2h_{i+3}}\right)e_{i+3} \\ 11) & \left(\frac{\pi}{2h_i}\right)^2(4\alpha_{i+1} + 2)q_i = \left(\frac{\pi}{2h_{i+1}}\right)^2[(4\alpha_{i+1} + 2)p_{i+1,0} - 4(\alpha_{i+1} + 2)p_{i+1,1} + 2(2 + \alpha_{i+1})p_{i+1,2} + 2(1 - \alpha_{i+1})p_{i+1,3}] \\ 12) & \left(\frac{\pi}{2h_{i+1}}\right)^2[(2 - 2\alpha_{i+1})p_{i+1,0} + 2(2 + \alpha_{i+1})p_{i+1,1} - 4(2 + \alpha_{i+1})p_{i+1,2} + (4\alpha_{i+1} + 2)p_{i+1,3}] = \left(\frac{\pi}{2h_{i+2}}\right)^2[(4\alpha_{i+2} + 2)f_{i+2,0} - (4\alpha_{i+2} + 8)f_{i+2,1} + (4 + 2\alpha_{i+3})f_{i+2,2} + (2 - 2\alpha_{i+3})f_{i+2,3}] \\ 13) & \left(\frac{\pi}{2h_{i+2}}\right)^2[(2 - \alpha_{i+2})f_{i+2,0} + 2(2 + \alpha_{i+2}) \cdot f_{i+2,1} - 4(2 + \alpha_{i+3})f_{i+2,2} + (2 + 4\alpha_{i+3})f_{i+2,3}] = \left(\frac{\pi}{2h_{i+3}}\right)^2(4\alpha_{i+3} + 2)e_{i+3} \end{aligned}$$

CR-B 样条基函数构建于函数空间 $T = \{s \in C^2[u_0, u_{n+4}], s_i = s|_{[u_i, u_{i+1}]} \in T_{\alpha_i, \beta_i}, i = 0, 1, \dots, n+3\}$, 式中, $T_{\alpha_i, \beta_i} = \text{span}\{1, 3t^2 - 2t^3, (1-t)^2(1-\alpha t), (1-\beta + \beta t)t^2\}$, $t_j(u) = (u - u_j)/h_j, j = 0,$

$1, \dots, n+3$ 。 $\text{span}()$ 为线性空间。当给定均匀节点矢量 U 以及 $\alpha_i = \alpha_{i+1} = \alpha_{i+2} = \alpha_{i+3}$ 时, CR-B 样条基为经典的非均匀三次 B 样条基。特别地, 对于 $u_{i+j} = u_i + jh, h > 0, j = 1, 2, 3, 4$ 时, 直接计算可得

$$\begin{aligned} q_i &= \frac{1}{6}; \quad p_{i+1,0} = \frac{1}{6}; \quad p_{i+1,1} = \frac{1}{3}; \quad p_{i+1,2} = \frac{2}{3}; \\ p_{i+1,3} &= \frac{2}{3}; \quad f_{i+1,0} = \frac{2}{3}; \quad f_{i+1,1} = \frac{2}{3}; \quad f_{i+1,2} = \frac{1}{3}; \\ f_{i+1,3} &= \frac{1}{6}; \quad e_{i+3} = \frac{1}{6} \end{aligned}$$

此时, CR-B 样条基为经典的均匀三次 B 样条基。

2.2 非均匀三次有理 B 样条基的性质

定理3 规范性: 对任意 $u \in [u_3, u_{n+1}]$,

$$\sum_{i=0}^n S_i(u) = 1.$$

证明: 对 $u \in [u_i, u_{i+1})$, $i = 3, 4, \dots, n$, 显然 $S_j(u) = 0, j \neq i-3, i-2, i-1, i$ 。由于

$$S_{i-3}(u) = e_i A_0(t_i; \alpha_i), S_{i-2}(u) = \sum_{j=0}^3 f_{i,j} A_j(t_i; \alpha_i)$$

$$S_{i-1}(u) = \sum_{j=0}^3 p_{i,j} A_j(t_i; \alpha_i), S_i(u) = q_i A_3(t_i; \alpha_i)$$

故利用引理1, 可得

$$\begin{aligned} \sum_{i=0}^n S_i(u) &= e_i A_0(t_i; \alpha_i) + \sum_{j=0}^3 f_{i,j} A_j(t_i; \alpha_i) + \\ &\sum_{j=0}^3 p_{i,j} A_j(t_i; \alpha_i) + q_i A_3(t_i; \alpha_i) = \sum_{j=0}^3 A_j(t_i; \alpha_i) = 1 \end{aligned}$$

定理4 非负性: 若 $\alpha_i \in [0, 1]$, 则对任意 $u_i < u < u_{i+4}$, 有 $S_i(u) > 0$ 。

证明: 对 $\alpha_i \in [0, 1]$, 显然 $e_i, f_{i,j}, p_{i,j}, q_i > 0$, 由 $A_j(t_i; \alpha_i), j = 0, 1, 2, 3$ 的非负性(陈福来等, 2012), 即可得 $S_i(u) > 0$ 。

定理5 线性无关性: 对任意 $\alpha_i \in [0, 1]$, $\{S_0(u), S_1(u), \dots, S_n(u)\}$ 在区间 $[u_3, u_{n+1}]$ 上线性无关。

证明: 取 $\zeta_i \in \mathbf{R}, i = 0, 1, \dots, n, u \in [u_3, u_{n+1}]$,

考虑 $S(u) = \sum_{i=0}^n \zeta_i S_i(u) = 0$, 对任意 $\alpha_i \in [0, 1]$,

有

$$S(u_i) = e_i \zeta_{i-3} + f_{i,0} \zeta_{i-2} + p_{i,0} \zeta_{i-1} = 0$$

$$S'(u_i) = \frac{1}{h_i}[(\alpha_i + 2)e_i(\zeta_{i-2} - \zeta_{i-3}) +$$

$$\frac{(\alpha_i + 2)q_{i-1}h_i}{h_{i-1}}(\zeta_{i-1} - \zeta_{i-2})] = 0$$

$$S''(u_i) = \left(\frac{1}{h_i}\right)^2[2(2\alpha_i + 1)e_i(\zeta_{i-3} - \zeta_{i-2}) +$$

$$\frac{2(2\alpha_i + 1)q_{i-1}h_i^2}{h_{i-1}^2}(\zeta_{i-1} - \zeta_{i-2})] = 0$$

式中, $i = 3, 4, \dots, n+1$ 。由此可得如下线性方程组成立

$$\begin{cases} e_i(\zeta_{i-3} - \zeta_{i-2}) + (e_i + f_{i,0} + p_{i,0})\zeta_{i-2} + \\ p_{i,0}(\zeta_{i-1} - \zeta_{i-2}) = 0 \\ - (a_i + 2)e_i(\zeta_{i-3} - \zeta_{i-2}) + \\ \frac{(\alpha_i + 2)q_{i-1}h_i}{h_{i-1}}(\zeta_{i-1} - \zeta_{i-2}) = 0 \\ (2\alpha_i + 1)e_i(\zeta_{i-3} - \zeta_{i-2}) + \\ \frac{(2\alpha_i + 1)q_{i-1}h_i^2}{h_{i-1}^2}(\zeta_{i-1} - \zeta_{i-2}) = 0 \end{cases}$$

由 $e_i + f_{i,0} + p_{i,0} = 1$, 则对应的系数行列式为

$$|M_i| = \begin{vmatrix} e_i & 1 & p_{i,0} \\ -(\alpha_i + 2)e_i & 0 & \frac{(\alpha_i + 2)q_{i-1}h_i}{h_{i-1}} \\ (2\alpha_i + 1)e_i & 0 & \frac{(2\alpha_i + 1)q_{i-1}h_i^2}{h_{i-1}^2} \end{vmatrix} = \frac{e_i q_{i-1} h_i}{h_{i-1}^2} (2\alpha_i + 1)(\alpha_i + 2)(h_i + h_{i-1}) > 0$$

因此, $\zeta_{i-3} = \zeta_{i-2} = \zeta_{i-1} = 0, i = 3, 4, \dots, n+1$ 。

定理6 全正性:对 $u \in [u_i, u_{i+1}]$, $\alpha_i \in [0, 1]$, $i = 3, 4, \dots, n$, $(S_{i-3}(u), S_{i-2}(u), S_{i-1}(u), S_i(u))$ 构成空间 T_{α_i} 中的一组规范全正基。

证明:对于 $u \in [u_i, u_{i+1}]$, $i = 3, 4, \dots, n$, 有 $(S_{i-3}(u), S_{i-2}(u), S_{i-1}(u), S_i(u)) = (A_0(t_i; \alpha_i), A_1(t_i; \alpha_i), A_2(t_i; \alpha_i), A_3(t_i; \alpha_i))H_i$, 式中,

$$H_i = \begin{bmatrix} e_i & f_{i,0} & p_{i,0} & 0 \\ 0 & f_{i,1} & p_{i,1} & 0 \\ 0 & f_{i,2} & p_{i,2} & 0 \\ 0 & f_{i,3} & p_{i,3} & q_i \end{bmatrix}$$

并且 $\alpha_i \in [0, 1]$, $t_i(u) = (u - u_i)/h_i$ 。

因为 $(A_0(t_i; \alpha_i), A_1(t_i; \alpha_i), A_2(t_i; \alpha_i), A_3(t_i; \alpha_i))$ 是函数空间 T_{α_i} 中的全正基, 因此要证明 $(S_{i-3}(u), S_{i-2}(u), S_{i-1}(u), S_i(u))$ 构成函数空间 T_{α_i} 中的一组规范全正基, 只需证明转换矩阵 H_i 是一个非奇异的随机全正矩阵。

对任意 $\alpha_i \in [0, 1]$, 明显有 $e_i, f_{i,j}, p_{i,j}, q_i > 0$ 成立。从引理1可以计算得出, H_i 的每一行相加总和等于1, 即 H_i 是随机矩阵。此外, 直接计算有

$$\begin{vmatrix} f_{i,0} & p_{i,0} \\ f_{i,1} & p_{i,1} \end{vmatrix} = \frac{\gamma_{i-1}h_i}{h_{i-1}}q_{i-2}q_{i-1} > 0$$

$$\begin{vmatrix} f_{i,0} & p_{i,0} \\ f_{i,2} & p_{i,2} \end{vmatrix} = \frac{h_i(3\sigma_{i-1}\tau_i h_{i+1} + \sigma_{i-1}\sigma_i h_i + 3\sigma_i\tau_{i-1}h_{i-1})}{9(\alpha_{i+1} + 2)\tau_{i-1}h_{i-1}h_{i+1}^2}e_{i+1}q_{i-1} + \frac{(\alpha_i + 2)\gamma_{i-1}\gamma_i h_i}{\tau_{i-1}}q_{i-2}q_{i-1} > 0$$

$$\begin{vmatrix} f_{i,0} & p_{i,0} \\ f_{i,3} & p_{i,3} \end{vmatrix} = \frac{(\alpha_i + 2)(\alpha_{i+1} + 2)\delta_i\delta_{i+1}h_{i-1}h_i}{\tau_{i-1}\tau_i}e_{i+1}e_{i+2} + \frac{h_i(3\sigma_{i-1}\tau_i h_{i+1} + \sigma_{i-1}\sigma_i h_i + 3\sigma_i\tau_{i-1}h_{i-1})}{9\tau_{i-1}\tau_i h_{i-1}h_{i+1}}e_{i+1}q_{i-1} + \frac{(\alpha_{i+1} + 2)(\alpha_i + 2)\sigma_{i+1}\gamma_{i-1}h_i^2}{\tau_{i-1}\tau_i}e_{i+2}q_{i-2} + \frac{(\alpha_i + 2)(\alpha_{i+1} + 2)\gamma_{i-1}\gamma_i h_i h_{i+1}}{\tau_{i-1}\tau_i}q_{i-2}q_{i-1} > 0$$

$$\begin{vmatrix} f_{i,1} & p_{i,1} \\ f_{i,2} & p_{i,2} \end{vmatrix} = \frac{h_i(3\sigma_{i-1}\tau_i h_{i+1} + \sigma_{i-1}\sigma_i h_i + 3\sigma_i\tau_{i-1}h_{i-1})}{9(\alpha_i + 2)(\alpha_{i+1} + 2)h_{i-1}^2 h_{i+1}^2}e_{i+1}q_{i-1} > 0$$

$$\begin{vmatrix} f_{i,1} & p_{i,1} \\ f_{i,3} & p_{i,3} \end{vmatrix} = \frac{h_i(3\sigma_{i-1}\tau_i h_{i+1} + \sigma_{i-1}\sigma_i h_i + 3\sigma_i\tau_{i-1}h_{i-1})}{9(\alpha_i + 2)\tau_i h_{i-1}^2 h_{i+1}}e_{i+1}q_{i-1} + \frac{(\alpha_{i+1} + 2)\delta_i\delta_{i+1}h_i}{\tau_i}e_{i+1}e_{i+2} > 0$$

$$\begin{vmatrix} f_{i,2} & p_{i,2} \\ f_{i,3} & p_{i,3} \end{vmatrix} = \frac{\delta_{i+1}h_i}{h_{i+1}}e_{i+1}e_{i+2} > 0$$

由此容易证明 H_i 为非奇异全正矩阵。

定理7 连续性:对任意非均匀节点向量 U 和 $i = 3, 4, \dots, n$, 当形状参数满足 $\alpha_i \in [0, 1]$ 时, 三次有理基函数 $S_i(u)$ 在每个节点处。

证明:要证明在每个节点处具有 C^2 连续, 不失一般性, 先讨论基在节点 u_{i+1} 处具有 C^2 连续, 对于任意的 $\alpha_i \in [0, 1]$, 计算可得

$$S_i(u_{i+1}^-) = q_i$$

$$S_i(u_{i+1}^+) = p_{i+1,0}$$

$$S_i'(u_{i+1}^-) = \frac{(\alpha_{i+1} + 2)q_i}{h_i}$$

$$S'_i(u_{i+1}^+) = \frac{(\alpha_{i+1} + 2)(p_{i+1,1} - p_{i+1,0})}{h_{i+1}}$$

$$S''_i(u_{i+1}^-) = \left(\frac{1}{h_i}\right)^2 (4\alpha_{i+1} + 2)q_i$$

$$S''_i(u_{i+1}^+) = \left(\frac{1}{h_{i+1}}\right)^2 [(4\alpha_{i+1} + 2)p_{i+1,0} - (4\alpha_{i+1} + 8)p_{i+1,1} + 2(2 + \alpha_{i+2})p_{i+1,2} + (2 - 2\beta_{i+1})p_{i+1,3}]$$

由上面的表达式和引理 1, 有 $S_i(u_{i+1}^+) = S_i(u_{i+1}^-)$, $S'_i(u_{i+1}^+) = S'_i(u_{i+1}^-)$, $S''_i(u_{i+1}^+) = S''_i(u_{i+1}^-)$, 由此定理可证。

推论 1 以上讨论都假定节点为单节点。现假定非均匀 CR-B 样条基 $S_i(u)$ 在节点 u_i 上具有重节点数 k , $k = 2, 3, 4, j = 2$, 则基 $S_i(u)$ 在该节点的连续性由 C^{j-1} 退化为 C^{j-k} (C^{-1} 表示不连续), 对照得出, 基 $S_i(u)$ 的支撑区间由 4 段退化为 $5 - k$ 。

3 非均匀加权 $\lambda\alpha\beta$ -B 样条

以三次有理基 $A_i(t)$ 和三次三角基 $B_i(t)$ 为工具, 结合加权思想, 对三次有理基 $A_i(t)$ 和三次三角

基 $B_i(t)$ 进行同时扩展, 得到新扩展基 $\lambda\alpha\beta$ -Bernstein 基, 用 $\lambda\alpha\beta$ -Bernstein 基的线性组合定义非均匀加权 $\lambda\alpha\beta$ -B 样条基, 并研究基和曲线的性质。

3.1 $\lambda\alpha\beta$ -Bernstein 基函数的构造

定义 3 对于 $\forall t \in [0, 1]$, $\alpha, \beta \in [0, 1]$, $\lambda \in [0, 1]$, $\lambda\alpha\beta$ -Bernstein 基的形式 $T_i(t) = \lambda A_i(t) + (1 - \lambda)B_i(t)$, 其中, $A_i(t)$ 和 $B_i(t)$ 分别为式(2)和式(1)定义的基函数, 即

$$\begin{cases} T_0(t) = \lambda(1-t)^2(1-\alpha t) + (1-\lambda)\left(1 - \sin \frac{\pi t}{2}\right)^2\left(1 - \beta \sin \frac{\pi t}{2}\right) \\ T_1(t) = \lambda(2+\alpha)t(1-t)^2 + (1-\lambda)\sin \frac{\pi t}{2}\left(1 - \sin \frac{\pi t}{2}\right)\left(2 + \beta - \beta \sin \frac{\pi t}{2}\right) \\ T_2(t) = \lambda(2+\alpha)t^2(1-t) + (1-\lambda)\cos \frac{\pi t}{2}\left(1 - \cos \frac{\pi t}{2}\right)\left(2 + \beta - \beta \cos \frac{\pi t}{2}\right) \\ T_3(t) = \lambda(1-\alpha+\alpha t)t^2 + (1-\lambda)\left(1 - \cos \frac{\pi t}{2}\right)^2\left(1 - \beta \cos \frac{\pi t}{2}\right) \end{cases} \quad (5)$$

图1是不同参数值下 $\lambda\alpha\beta$ -Bernstein 基的图

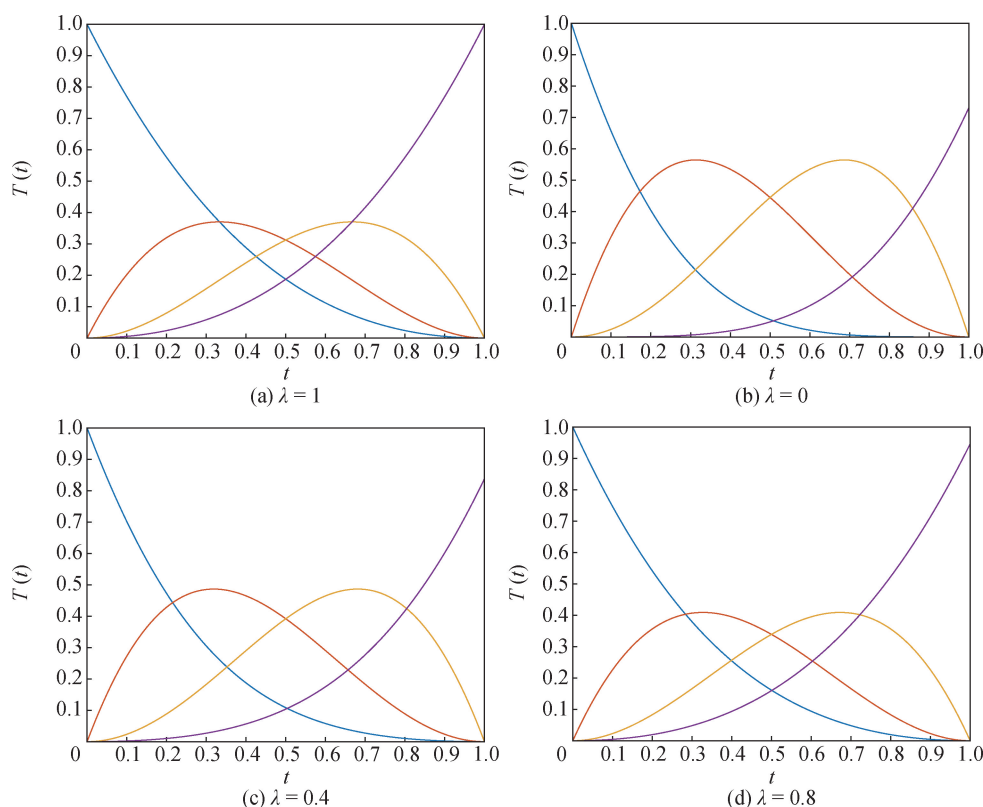


图1 $\lambda\alpha\beta$ -Bernstein 基在不同参数值下的图像

Fig. 1 Images of $\lambda\alpha\beta$ -Bernstein basis under different parameter values ((a) $\lambda = 1$; (b) $\lambda = 0$; (c) $\lambda = 0.4$; (d) $\lambda = 0.8$)

像。其中,当 $\lambda = 1$ 时为三次有理基 $A_i(t)$ 的图像,当 $\lambda = 0$ 时为三次三角基 $B_i(t)$ 的图像,当 $\lambda \neq 0$ 且 $\lambda \neq 1$ 时,为 $\lambda\alpha\beta$ -Bernstein 基的图像,其中 α 和 β 取固定值, $\alpha = \beta = 1/2$, λ 分别取 0.4 和 0.8。

3.2 非均匀加权 $\lambda\alpha\beta$ -B 样条基的定义与性质

由于 $\lambda\alpha\beta$ -Bernstein 基定义的曲线在控制顶点固定的情况下不具有形状可调性,且未能解决描述复杂曲线时的光滑拼接问题,为此在式(5)的基础上,构造一类非均匀加权 $\lambda\alpha\beta$ -B 样条基(简称 $\lambda\alpha\beta$ -B 样条基)进行曲线设计。

对于给定的节点序列 $u_0 < u_1 < \dots < u_{n+4}$,记为节点矢量 $\mathbf{U} = (u_0, u_1, \dots, u_{n+4})$ 。令

$$h_j = u_{j+1} - u_j, t_j(u) = (u - u_j)/h_j, \\ j = 0, 1, \dots, n+3$$

对于任意的形状参数 $\alpha_i, \beta_i \in [0, 1], i = 0, 1, \dots, n$,待构造的 $\lambda\alpha\beta$ -B 样条基为

$$D_i(u) = \begin{cases} D_{i,0}(t_i) = d_i T_3(t_i; \lambda_i, \alpha_i, \beta_i) & u \in [u_i, u_{i+1}) \\ D_{i,1}(t_{i+1}) = \\ \sum_{j=0}^3 c_{i+1,j} T_j(t_{i+1}; \lambda_{i+1}, \alpha_{i+1}, \beta_{i+1}) & u \in [u_{i+1}, u_{i+2}) \\ D_{i,2}(t_{i+2}) = \\ \sum_{j=0}^3 b_{i+2,j} T_j(t_{i+2}; \lambda_{i+2}, \alpha_{i+2}, \beta_{i+2}) & u \in [u_{i+2}, u_{i+3}) \\ D_{i,3}(t_{i+3}) = \\ a_{i+3} T_0(t_{i+3}; \lambda_{i+3}, \alpha_{i+3}, \beta_{i+3}) & u \in [u_{i+3}, u_{i+4}) \\ 0 & u \notin [u_i, u_{i+4}) \end{cases} \quad (6)$$

式中, $T_j(t_i; \lambda_i, \alpha_i, \beta_i) (j = 0, 1, 2, 3)$ 为式(5)中给出的基函数。

为了确定系数 $a_i, b_{i,j}, c_{i,j}, d_i$ 的值,对构造的 $\lambda\alpha\beta$ -B 样条基进行限制:1) $D_i(u)$ 在所有节点上均有 C^2 连续;2) $D_i(u)$ 在区间 $[u_3, u_{n+1}]$ 上具有单位性。由此经过运算后,可以直接求出系数为

$$\theta_i = [\lambda(2\alpha_{i+1} + 1)(\alpha_{i+1} + 2) + \\ (1 - \lambda)(2\beta_i + 1)(\beta_i + 2)](h_i + h_{i+1}) \\ \eta_i = [\lambda(\alpha_{i+1} + 2) + (1 - \lambda)(\beta_i + 2)](h_i + h_{i+1}) \\ \varphi_i = \lambda \frac{\sigma_i h_i + 3\tau_i h_{i+1}}{3(\alpha_{i+1} + 2)h_{i+1}^2} + (1 - \lambda) \frac{\mu_i h_i + \nu_i h_{i+1}}{(\beta_i + 2)h_{i+1}^2} \\ \phi_i = \lambda \frac{\sigma_{i-1} h_i + 3\tau_{i-1} h_{i-1}}{3(\alpha_i + 2)h_{i-1}^2} + (1 - \lambda) \frac{\mu_{i-1} h_i + \nu_{i-1} h_{i-1}}{(\beta_{i-1} + 2)h_{i-1}^2}$$

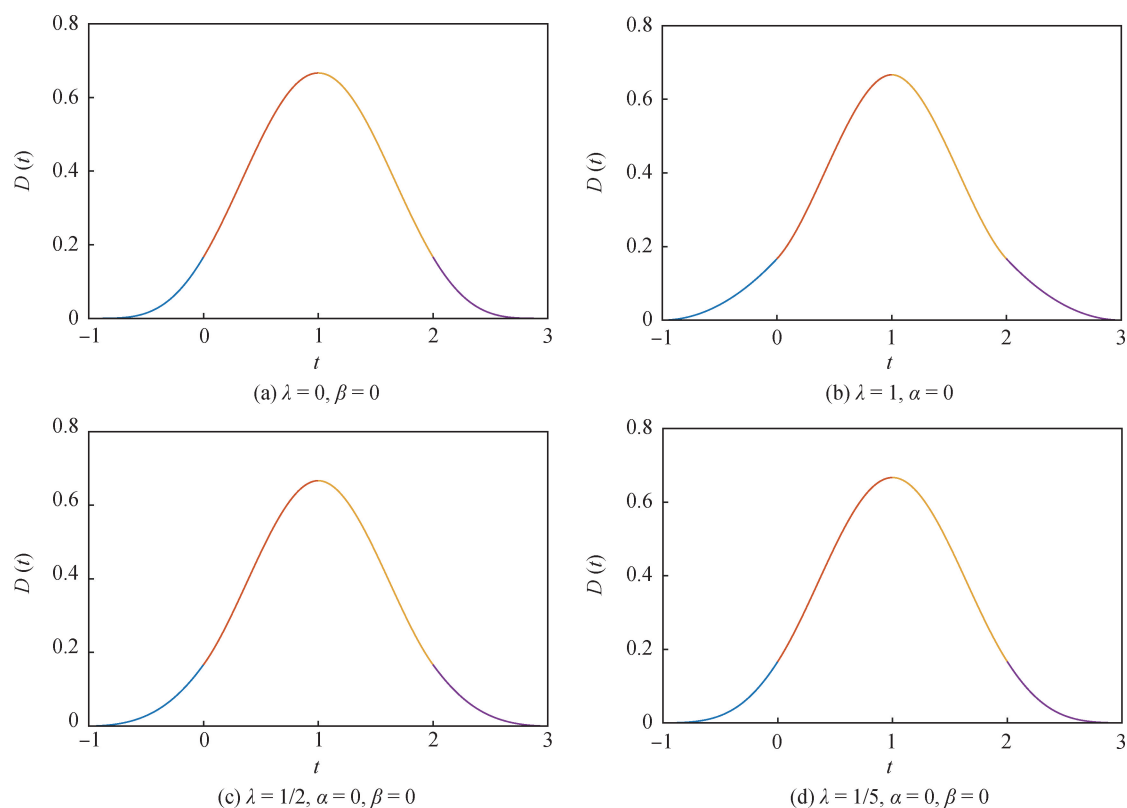
$$a_i = \lambda \frac{3(\alpha_i + 2)\sigma_{i-2} h_i^2}{3\sigma_{i-1}\tau_{i-2}h_{i-2} + \sigma_{i-2}\sigma_{i-1}h_{i-1} + 3\sigma_{i-2}\tau_{i-1}h_i} + \\ (1 - \lambda) \frac{(\beta_{i-1} + 2)\mu_{i-2} h_i^2}{\mu_{i-1}\nu_{i-2}h_{i-2} + \mu_{i-2}\mu_{i-1}h_{i-1} + \mu_{i-2}\nu_{i-1}h_i} \\ d_i = \lambda \frac{3(\alpha_{i+1} + 2)\sigma_{i+1} h_i^2}{3\sigma_{i+1}\tau_i h_i + \sigma_i\sigma_{i+1}h_{i+1} + 3\sigma_i\tau_{i+1}h_{i+2}} + \\ (1 - \lambda) \frac{(\beta_i + 2)\mu_{i+1} h_i^2}{\mu_{i+1}\nu_i h_i + \mu_i\mu_{i+1}h_{i+1} + \mu_i\nu_{i+1}h_{i+2}} \\ b_{i,0} = \lambda \left[\frac{(\alpha_i + 2)\delta_i h_{i-1}}{\tau_{i-1}} e_{i+1} + \frac{(\alpha_i + 2)\gamma_{i-1} h_i}{\tau_{i-1}} q_{i-2} \right] + \\ (1 - \lambda) \left[\frac{(\beta_{i-1} + 2)\nu_{i-1} h_{i-1}}{\nu_{i-1}} x_{i+1} + \frac{(\beta_{i-1} + 2)\omega_{i-1} h_i}{\nu_{i-1}} n_{i-2} \right] \\ b_{i,1} = \lambda \delta_i e_{i+1} + (1 - \lambda) \nu_i x_{i+1} \\ c_{i,0} = \lambda q_{i-1} + (1 - \lambda) n_{i-1} \\ b_{i,2} = \lambda \frac{\tau_i}{(\alpha_{i+1} + 2)h_{i+1}} e_{i+1} + (1 - \lambda) \frac{\nu_i}{(\beta_i + 2)h_{i+1}} x_{i+1} \\ c_{i,1} = \lambda \frac{\tau_{i-1}}{(\alpha_i + 2)h_{i-1}} q_{i-1} + (1 - \lambda) \frac{\nu_{i-1}}{(\beta_{i-1} + 2)h_{i-1}} n_{i-1} \\ b_{i,3} = \lambda e_{i+1} + (1 - \lambda) x_{i-1} \\ c_{i,2} = \lambda \gamma_i q_{i-1} + (1 - \lambda) \omega_i n_{i-1} \\ c_{i,3} = \lambda \left[\frac{(\alpha_{i+1} + 2)\delta_{i+1} h_i}{\tau_i} e_{i+2} + \frac{(\alpha_{i+1} + 2)\gamma_i h_{i+1}}{\tau_i} q_{i-1} \right] + \\ (1 - \lambda) \left[\frac{(\beta_i + 2)\nu_{i+1} h_i}{\nu_i} x_{i+2} + \frac{(\beta_i + 2)\omega_i h_{i+1}}{\nu_i} n_{i-1} \right]$$

定义4 给定的节点矢量 $\mathbf{U}$,对于任意 $\alpha_i, \beta_i \in [0, 1]$ 和上面给出的系数 $a_i, b_{i,j}, c_{i,j}, d_i$,称式(6)为带3个参数的 $\lambda\alpha\beta$ -B 样条基。

当节点矢量为等距节点时,称 $\lambda\alpha\beta$ -B 样条基 $D_i(u)$ 为均匀 $\lambda\alpha\beta$ -B 样条基。图2是取不同的参数值时,均匀 $\lambda\alpha\beta$ -B 样条基 $D_i(u)$ 的图像。

引理2 对任意 $i \in \mathbf{Z}$,下列等式成立

$$\begin{aligned} 1) & a_i + b_{i,0} + c_{i,0} = 1 \\ 2) & b_{i,1} + c_{i,1} = 1 \\ 3) & b_{i,2} + c_{i,2} = 1 \\ 4) & b_{i,3} + c_{i,3} + d_i = 1 \\ 5) & d_i = c_{i+1,0} \\ 6) & b_{i+2,0} = c_{i+1,3} \\ 7) & b_{i+2,3} = a_{i+3} \\ 8) & \frac{1}{h_i} \left[\lambda_i(2 + \alpha_i) + \frac{\pi}{2}(1 - \lambda_i)(2 + \beta_i) \right] d_i = \\ & \frac{1}{h_{i+1}} \left[\lambda_{i+1}(2 + \alpha_{i+1}) + \frac{\pi}{2}(1 - \lambda_{i+1})(2 + \beta_{i+1}) \right] \cdot \\ & (c_{i+1,1} - c_{i+1,0}) \end{aligned}$$

图2 均匀 $\lambda\alpha\beta$ -B 样条基图像Fig. 2 Images of uniform $\lambda\alpha\beta$ -B-spline bases

((a) $\lambda = 0, \beta = 0$; (b) $\lambda = 1, \alpha = 0$; (c) $\lambda = 1/2, \alpha = 0, \beta = 0$; (d) $\lambda = 1/5, \alpha = 0, \beta = 0$)

9)

$$\frac{1}{h_{i+1}} \left[\lambda_{i+1}(2 + \alpha_{i+1}) + \frac{\pi}{2}(1 - \lambda_{i+1})(2 + \beta_{i+1}) \right] \cdot (c_{i+1,3} - c_{i+1,2}) =$$

$$\frac{1}{h_{i+2}} \left[\lambda_{i+2}(2 + \alpha_{i+2}) + \frac{\pi}{2}(1 - \lambda_{i+2})(2 + \beta_{i+2}) \right] \cdot (b_{i+2,1} - b_{i+2,0})$$

10)

$$\frac{1}{h_{i+2}} \left[\lambda_{i+2}(2 + \alpha_{i+2}) + \frac{\pi}{2}(1 - \lambda_{i+2})(2 + \beta_{i+2}) \right] \cdot (b_{i+2,3} - b_{i+2,2}) =$$

$$-\frac{1}{h_{i+3}} \left[\lambda_{i+3}(2 + \alpha_{i+3}) + \frac{\pi}{2}(1 - \lambda_{i+3})(2 + \beta_{i+3}) \right] \cdot$$

 a_{i+3}

$$11) \left(\frac{1}{h_i} \right)^2 \left[\lambda_i(2 + 4\alpha_i) + (1 - \lambda_i)\pi^2(\beta_i + 1/2) \right] d_i =$$

$$\left(\frac{1}{h_{i+1}} \right)^2 \left\{ [\lambda_{i+1}(2 + 4\alpha_{i+1}) + (1 - \lambda_{i+1})\pi^2(\beta_{i+1} + 1/2)] c_{i+1,0} - [4\lambda_{i+1}(2 + \alpha_{i+1}) + (1 - \lambda_{i+1})(1 + \beta_{i+1})\pi^2] c_{i+1,1} + [4\lambda_{i+1}(1 + \alpha_{i+1}) + (1 - \lambda_{i+1}) \cdot \right.$$

$$\frac{\pi^2}{2} c_{i+1,2} + [2\lambda_{i+1}(1 - \alpha_{i+1})] c_{i+1,3} \}$$

$$12) \left(\frac{1}{h_{i+1}} \right)^2 \left\{ [2\lambda_{i+1}(1 - \alpha_{i+1}) c_{i+1,0} + [2\lambda_{i+1}(2 + \alpha_{i+1}) + (1 - \lambda_{i+1}) \frac{\pi^2}{2}] c_{i+1,1} - [\lambda_{i+1}4(2 + \alpha_{i+1}) + (1 - \lambda_{i+1})(1 + \beta_{i+1})\pi^2] c_{i+1,2} + [2\lambda_{i+1}(1 + 2\alpha_{i+1}) + (1 - \lambda_{i+1})(\beta_{i+1} + 1/2)\pi^2] c_{i+1,3} \} =$$

$$\left(\frac{1}{h_{i+2}} \right)^2 \left\{ [2\lambda_{i+2}(1 + 2\alpha_{i+2}) + (1 - \lambda_{i+2})(\beta_{i+2} + 1/2)\pi^2] b_{i+2,0} - [\lambda_{i+2}4(2 + \alpha_{i+2}) + (1 - \lambda_{i+2})(1 + \beta_{i+2})\pi^2] b_{i+2,1} + [\lambda_{i+2}2(2 + \alpha_{i+2}) + (1 - \lambda_{i+2}) \frac{\pi^2}{2}] b_{i+2,2} + [\lambda_{i+2}(2 - 2\alpha_{i+2})] b_{i+2,3} \}$$

$$13) \left(\frac{1}{h_{i+2}} \right)^2 \left\{ [\lambda_{i+2}(2 - 2\alpha_{i+2})] b_{i+2,0} + [\lambda_{i+2}2(2 + \alpha_{i+2}) + (1 - \lambda_{i+2}) \frac{\pi^2}{2}] b_{i+2,1} - [\lambda_{i+2}4(2 + \alpha_{i+2}) + (1 - \lambda_{i+2})(1 + \beta_{i+2})\pi^2] b_{i+2,2} + [2\lambda_{i+2}(1 + 2\alpha_{i+2}) + (1 - \lambda_{i+2})(\beta_{i+2} + 1/2)\pi^2] b_{i+2,3} \} =$$

$$\left(\frac{1}{h_{i+3}}\right)^2 [\lambda_{i+3}(2 + 4\alpha_{i+3}) + (1 - \lambda_{i+3})(\beta_{i+3} + 1/2)\pi^2] a_{i+3}$$

当 $\lambda = 1$ 时, 上述所求系数是三次有理 B 样条基的系数; 当 $\lambda = 0$ 时, 所求系数是三次三角 B 样条基的系数。此时, 给定一个均匀节点矢量, 当形状参数满足 $\beta_i \in [0, 1]$ 时, CT-B 样条基 $G_i(u)$ 在每个节点处满足 C^{2n-1} ($n = 1, 2, 3, \dots$) 高阶连续性, 而且 CT-B 样条曲线在每个节点处也满足 C^{2n-1} ($n = 1, 2, 3, \dots$) 高阶连续性。

由于用来构造非均匀加权 $\lambda\alpha\beta$ -B 样条基的 $\lambda\alpha\beta$ -Bernstein 基函数是三次有理基和三次三角基加权得到的, 所以非均匀加权 $\lambda\alpha\beta$ -B 样条基具有 CT-B 样条基和 CR-B 样条基相似的性质, 即具有规范性、非负性、线性无关性、全正性和连续性。

3.3 非均匀加权 $\lambda\alpha\beta$ -B 样条曲线

3.3.1 非均匀加权 $\lambda\alpha\beta$ -B 样条曲线的定义与性质

定义 5 给定非均匀节点矢量 U 和控制点 W_i ($i = 0, 1, \dots, n$) $\in \mathbf{R}^2/\mathbf{R}^3$, $n \geq 3$, 对任意的 $\alpha_i, \beta_i \in [0, 1]$, $n \geq 3$, $u \in [u_3, u_{n+1}]$, 称

$$W(u) = \sum_{i=0}^n D_i(u) W_i$$

为非均匀加权 $\lambda\alpha\beta$ -B 样条曲线 (简称 $\lambda\alpha\beta$ -B 样条曲线)。

显然, 对于 $u \in [u_i, u_{i+1}]$, $i = 3, 4, \dots, n$, $\lambda\alpha\beta$ -B 样条曲线段 $W_i(u)$ 可表示为

$$\begin{aligned} W(u) = & \sum_{j=i-3}^i D_j(u) W_j = \\ & (a_i W_{i-3} + b_{i0} W_{i-2} + c_{i0} W_{i-1}) T_0(t_i; \lambda_i, \alpha_i, \beta_i) + \\ & (b_{i1} W_{i-2} + c_{i1} W_{i-1}) T_1(t_i; \lambda_i, \alpha_i, \beta_i) + \\ & (b_{i2} W_{i-2} + c_{i2} W_{i-1}) T_2(t_i; \lambda_i, \alpha_i, \beta_i) + \\ & (b_{i3} W_{i-2} + c_{i3} W_{i-1} + d_i W_i) T_3(t_i; \lambda_i, \alpha_i, \beta_i) \end{aligned} \quad (7)$$

从基函数 $D_i(u)$ 的权性和非负性可知, $\lambda\alpha\beta$ -B 样条曲线 $W(u)$ 具有仿射不变性, 且对 $u \in [u_i, u_{i+1}]$, $i = 3, 4, \dots, n$, $W(u)$ 位于控制顶点 $W_{i-3}, W_{i-2}, W_{i-1}, W_i$ 形成的凸包之内。此外, 从基 $D_i(u)$ 的全正性可以看出, 曲线 $W(u)$ 具有重要的变差缩减性。这意味着曲线 $W(u)$ 适用于曲线设计。由基函数的连续性, 可直接得到如下定理。

定理 8 对任意非等距节点向量 U 和 $i = 3, 4, \dots, n$, 如果节点 u_i 具有 k 重, 则非均匀 $\lambda\alpha\beta$ -B 样

条基 $D_i(u)$ 在该节点上为 C^{j-k} 连续, 其中对 $\alpha_i, \beta_i \in [0, 1]$, $k = 2, 3, 4, j = 2$ 。此外, 对单节点 u_i 有

$$\begin{aligned} W(u_i) = & [\lambda e_i + (1 - \lambda)x_i] W_{i-3} + \\ & [\lambda f_{i,0} + (1 - \lambda)y_{i,0}] W_{i-2} + \\ & [\lambda p_{i,0} + (1 - \lambda)m_{i,0}] W_{i-1} \end{aligned} \quad (8)$$

$$\begin{aligned} W'(u_i) = & \frac{1}{h_i} \{ [\lambda(\alpha_i + 2)e_i + (1 - \lambda)(\beta_{i-1} + 2)x_i] \cdot \\ & (W_{i-2} - W_{i-3}) + \\ & \frac{[\lambda(\alpha_i + 2)q_{i-1} + (1 - \lambda)(\beta_{i-1} + 2)n_{i-1}] h_i}{h_{i-1}} \\ & (W_{i-1} - W_{i-2}) \} \end{aligned} \quad (9)$$

$$\begin{aligned} W''(u_i) = & \left(\frac{1}{h_i}\right)^2 \{ [2\lambda(2\alpha_i + 1)e_i + 2(1 - \lambda) \cdot \\ & (2\beta_{i-1} + 1)x_i] (W_{i-3} - W_{i-2}) + \\ & \frac{[2\lambda(2\alpha_i + 1)q_{i-1} + 2(1 - \lambda)(2\beta_{i-1} + 1)n_{i-1}] h_i^2}{h_{i-1}^2} \\ & (W_{i-1} - W_{i-2}) \} \end{aligned} \quad (10)$$

3.3.2 $C^2 \cap FC^{k+3}$ 连续曲线

由 $\lambda\alpha\beta$ -Bernstein 基 $T_j(t_i; \lambda_i, \alpha_i, \beta_i)$, $j = 0, 1, 2, 3$ 的端点性质, 依据朱远鹏 (2014) 提出的拟三次非均匀 B 样条 $C^2 \cap FC^{k+3}$ 连续曲线, 可得如下定理。

定理 9 对 $k \in \mathbf{Z}^+$, 如果形状参数 $\alpha_i, \beta_i \in [0, 1]$ 且 u_i 为单节点, 则非均匀 $\lambda\alpha\beta$ -B 样条曲线 $W(u)$ 在该节点上达到 $C^2 \cap FC^{k+3}$ 连续。

证明: 对任意 $\alpha_i, \beta_i \in [0, 1]$, 由式 (9) 和式 (10) 可得

$$\begin{aligned} W_{i-1} - W_{i-2} = & \frac{[2\lambda(2\alpha_i + 1)e_i + 2(1 - \lambda)(2\beta_{i-1} + 1)x_i] h_i}{|M_i|} \cdot \\ & W'(u_i) + \\ & \frac{[\lambda(\alpha_i + 2)e_i + (1 - \lambda)(\beta_{i-1} + 2)x_i] h_i^2}{|M_i|} \cdot \\ & W''(u_i) \\ W_{i-2} - W_{i-3} = & \frac{[2\lambda(2\alpha_i + 1)q_{i-1} + 2(1 - \lambda)(2\beta_{i-1} + 1)n_{i-1}] h_i^3}{h_{i-1}^2 |M_i|} \cdot \\ & W'(u_i) - \\ & \frac{[\lambda(\alpha_i + 2)q_{i-1} + (1 - \lambda)(\beta_{i-1} + 2)n_{i-1}] h_i^3}{h_{i-1} |M_i|} W''(u_i) \end{aligned}$$

式中,

$$|M_i| =$$

$$\frac{1}{h_{i-1}^2} \{ [\lambda(\alpha_i + 2)q_{i-1} + (1 - \lambda)(\beta_{i-1} + 2)n_{i-1}] \cdot$$

$$\begin{aligned} & [\lambda(\alpha_i + 2)e_i + (1 - \lambda)(\beta_{i-1} + 2)x_i]h_i^2 + \\ & [\lambda(\alpha_i + 2)q_{i-1} + (1 - \lambda)(\beta_{i-1} + 2)n_{i-1}] \cdot \\ & [2\lambda(2\alpha_i + 1)e_i + 2(1 - \lambda)(2\beta_{i-1} + 1)x_i]h_i h_{i-1} \} \end{aligned} \quad (11)$$

$$\begin{aligned} W^{(j)}(u_i^+) - W^{(j)}(u_i^-) = & \left[\left(\frac{1}{h_i} \right)^j D_{i-3,3}^{(j)}(0) - \left(\frac{1}{h_{i-1}} \right)^j D_{i-3,2}^{(j)}(1) \right] W_{i-3} + \\ & \left[\left(\frac{1}{h_i} \right)^j D_{i-2,2}^{(j)}(0) - \left(\frac{1}{h_{i-1}} \right)^j D_{i-2,1}^{(j)}(1) \right] W_{i-2} + \\ & \left[\left(\frac{1}{h_i} \right)^j D_{i-1,1}^{(j)}(0) - \left(\frac{1}{h_{i-1}} \right)^j D_{i-1,0}^{(j)}(1) \right] W_{i-1} \end{aligned} \quad (12)$$

由三次有理基 $T_j(t_i; \lambda_i, \alpha_i, \beta_i)$, $j = 0, 1, 2, 3$ 的端点性质可得

$$\begin{aligned} & \left[\left(\frac{1}{h_i} \right)^j D_{i-3,3}^{(j)}(0) - \left(\frac{1}{h_{i-1}} \right)^j D_{i-3,2}^{(j)}(1) \right] + \\ & \left[\left(\frac{1}{h_i} \right)^j D_{i-2,2}^{(j)}(0) - \left(\frac{1}{h_{i-1}} \right)^j D_{i-2,1}^{(j)}(1) \right] + \\ & \left[\left(\frac{1}{h_i} \right)^j D_{i-1,1}^{(j)}(0) - \left(\frac{1}{h_{i-1}} \right)^j D_{i-1,0}^{(j)}(1) \right] = \\ & \left(\frac{1}{h_i} \right)^j [T_0^{(j)}(0; \alpha_i) + T_1^{(j)}(0; \alpha_i) + T_2^{(j)}(0; \alpha_i)] - \\ & \left(\frac{1}{h_{i-1}} \right)^j [T_1^{(j)}(1; \alpha_i) + T_2^{(j)}(1; \alpha_i) + T_3^{(j)}(1; \alpha_i)] = \\ & \left(\frac{1}{h_i} \right)^j \times 0 - \left(\frac{1}{h_{i-1}} \right)^j \times 0 = 0 \end{aligned}$$

因此,将式(12)改写为

$$\begin{aligned} W^{(j)}(u_i^+) - W^{(j)}(u_i^-) = & \left[\left(\frac{1}{h_i} \right)^j D_{i-1,1}^{(j)}(0) - \left(\frac{1}{h_{i-1}} \right)^j D_{i-1,0}^{(j)}(1) \right] (W_{i-1} - W_{i-2}) + \\ & \left[- \left(\frac{1}{h_i} \right)^j D_{i-3,3}^{(j)}(0) - \left(\frac{1}{h_{i-1}} \right)^j D_{i-3,2}^{(j)}(1) \right] \cdot \\ & (W_{i-2} - W_{i-3}) : = \end{aligned}$$

$$\tau_{i,j}(W_{i-1} - W_{i-2}) + \sigma_{i,j}(W_{i-2} - W_{i-3})$$

利用式(11),进一步可得

$$\begin{aligned} W^{(j)}(u_i^+) - W^{(j)}(u_i^-) = & \left[\frac{(\alpha_i + 2)e_i h_i^2}{|M_i|} \tau_{i,j} - \frac{(\alpha_i + 2)q_{i-1} h_i^3}{h_{i-1} |M_i|} \sigma_{i,j} \right] W''(u_i) + \\ & \left[\frac{2(2\alpha_i + 2)e_i h_i}{|M_i|} + \frac{2(2\alpha_i + 1)q_{i-1} h_{i-1}^3}{h_{i-1}^2 |M_i|} \right] W'(u_i) : = \\ & \omega_{i,j}^{(2)} W''(u_i) + \omega_{i,j}^{(1)} W'(u_i) \end{aligned}$$

3.3.3 局部调整性质

由朱远鹏(2014)提出的拟三次三角非均匀 B 样条的局部调整性质可知, $\lambda\alpha\beta$ -B 样条曲线 $W(u)$

中含 3 个局部形状参数 $\lambda_i, \alpha_i, \beta_i$, 在不改变控制点下, 可以通过改变形状参数值对 $\lambda\alpha\beta$ -B 样条曲线进行局部调整。由式(7)可知, 形状参数 λ 可以决定曲线的类型, 当 $\lambda = 1$ 时是三次有理 B 样条曲线, 当 $\lambda = 0$ 时是三次三角 B 样条曲线, 当 $\lambda \neq 0$ 且 $\lambda \neq 1$ 时, $\alpha_{i-1}, \alpha_i, \alpha_{i+1}, \alpha_{i+2}, \beta_{i-2}, \beta_{i-1}, \beta_i, \beta_{i+1}$ 影响曲线段 $W(u)$, $u \in [u_i, u_{i+1}]$ 的形状。换言之, 形状参数 α_i 影响参数区间为 $[u_{i-2}, u_{i+2}]$ 的 4 段曲线形状, 而形状参数 β_i 影响参数区间为 $[u_{i-1}, u_{i+3}]$ 的 4 段曲线形状。此外, 可以预测曲线 $W(u)$ 随形状参数取值的形状变化趋势。随着 α_i 和 β_i 的增加, 控制点 W_{i-3} 和 W_i 的系数减小, 而控制点 W_{i-2} 和 W_{i-1} 的系数增大。从而, 随着 α_i 和 β_i 同时增加, 曲线 $W(u)$ 趋向边 $W_{i-2}W_{i-1}$; α_i 或 β_i 增加, 曲线 $W(u)$ 将分别趋向控制点 W_{i-2} 和 W_{i-1} 。

图 3 是均匀 $\lambda\alpha\beta$ -B 样条曲线。图 3(a) 是当 $\lambda = 1$ 时, 分别取 $\alpha_i = 0$ 和 $\alpha_i = 1$, 此时是三次有理 B 样条曲线的图像; 图 3(b) 是当 $\lambda = 0$ 时, 分别取 $\beta_i = 0$ 和 $\beta_i = 1$, 此时是三次三角 B 样条曲线的图像; 图 3(c) 和图 3(d) 是分别固定形状参数 $\lambda_i = 1/2$ 和 $\lambda_i = 1/5$ 时, 均匀 $\lambda\alpha\beta$ -B 样条曲线的图像。蓝色实线是 $\alpha = \beta = 0$ 时的情形, 黑色虚线是 $\alpha = 0, \beta = 1$ 时的情形, 红色虚线是 $\alpha = 1, \beta = 0$ 时的情形, 绿色虚线是 $\alpha_i = \beta_i = 1$ 时的情形。

3.3.4 $\lambda\alpha\beta$ -B 样条曲线的应用

由于结合加权法的 $\lambda\alpha\beta$ -B 样条曲线既保留了有理多项式的性质, 又保留了三角多项式的性质, 因此可以用来表示二次曲线。图 4 是当 $\alpha = 0, \beta = 0, \lambda = 1/2$ 时的椭圆图像。

4 结 论

本文研究的主要内容是鉴于传统文献在有理基和三角基对 B 样条方法进行改进时控制顶点较为固定的不足, 在保留多项式空间和三角函数空间优点的同时, 利用加权法对这两个函数空间构造的基函数进行整合, 定义了一种非均匀加权 $\lambda\alpha\beta$ -B 样条基, 并引入新的加权因子, 进行曲线构造。主要结果是构造的非均匀加权 $\lambda\alpha\beta$ -B 样条曲线具有局部调整性, 可以改善只通过调整控制顶点来改变曲线形状的不足, 同时可以用来表示二次曲线。本文研究

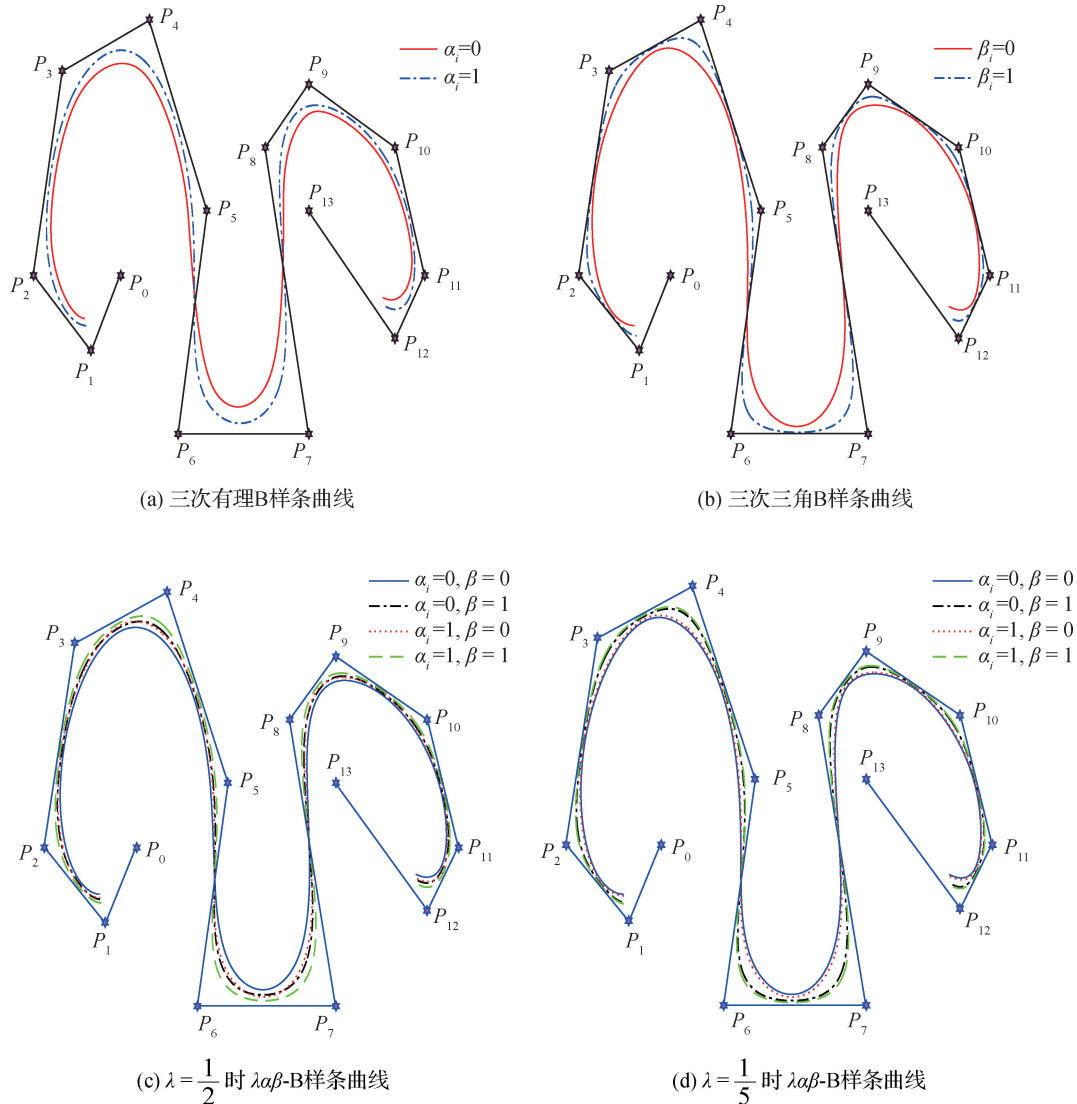
图3 均匀 $\lambda\alpha\beta$ -B 样条曲线

Fig. 3 Uniform $\lambda\alpha\beta$ -B-spline curve ((a) cubic rational B-spline curve; (b) cubic trigonometric B-spline; (c) $\lambda\alpha\beta$ -B-spline when $\lambda = 1/2$; (d) $\lambda\alpha\beta$ -B-spline when $\lambda = 1/5$)

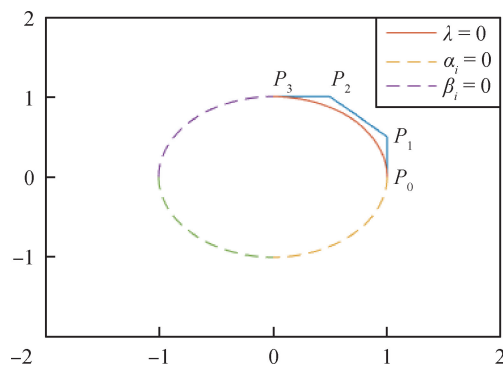


图4 椭圆
Fig. 4 Ellipse

方法与其他方法比较的优点在于分析解决了传统文献在改进时遗留的问题,适于曲线设计。但是也存在

在不足,本文只探讨了三次非均匀 B 样条,对于高阶非均匀 B 样条并未研究,曲线的尖点、拐点等问题也未描述。同时,如何将 $\lambda\alpha\beta$ -B 样条曲线推广到 $\lambda\alpha\beta$ -B 样条曲面等问题也没有讨论。为了设计出更加符合几何工业实际需求的造型,对曲线的构造仍有很多值得研究的问题。

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